

**UTAH DIVISION OF AIR QUALITY**  
**MODIFIED SOURCE PLAN REVIEW**

George W. Cross, President  
 Intermountain Power Service Corporation  
 850 West Brush Wellman Road  
 Delta, Utah 84624 RE:

Project fee code: N0327-010

REVIEW ENGINEER:

DATE:

NOTICE OF INTENT SUBMITTED:

PLANT CONTACT:

PHONE NUMBERS:

FAX NUMBER:

SOURCE LOCATION:

UTM COORDINATES:

CO PSD Major Modification to DAQE-049-02 at Unit 1 and 2  
 Intermountain Generating Station  
 Millard County, Utah CDS-A, ATT, Title V, Title IV, NSPS  
 Milka M. Radulovic  
 April 30, 2003  
 November 4, 2002 & March 24, 2003  
 Rand Crafts  
 (435) 864-6494  
 (435) 864-0994  
 850 West Brush Wellman Road Delta, Millard County, Utah  
 4,374.4 km Northing, 364.2 km Easting, Zone 12 datum  
 NAD27

REVIEW:

Peer Engineer \_\_\_\_\_

John Jenks

DAQ requests that a company/corporation official read the attached draft/proposed Plan Review with Recommended Approval Order Conditions. If this person does not understand or does not agree with the conditions, the PLAN REVIEW ENGINEER should be contacted within five days after receipt of the Plan Review. Special attention needs to be addressed to the Recommended AO Conditions because they will be recommended for the final AO. If this person understands and the company/corporation agrees with the Plan Review or Recommended AO Conditions, this person should sign below and return (can use FAX # 801-536-4099) within 10 days after receipt of the conditions. If the Plan Review Engineer is not contacted within 10 days, the Plan Review Engineer shall assume that the Company/Corporation official agrees with this Plan Review and will process the Plan Review towards final approval. A 30-day public comment period will be required before the Approval Order can be issued.

Thank You

Applicant Contact \_\_\_\_\_

(Signature & Date)

**OPTIONAL:** In order for this Source Plan Review and associated Approval Order conditions to be administratively included in your Operating Permit (Application), the Responsible Official as defined in R307-415-3, must sign the statement below and the signature above is not necessary. **THIS IS STRICTLY OPTIONAL!** If you do not desire this Plan Review to be administratively included in your Operating Permit (Application), only the Applicant Contact signature above is required. Failure to have the Responsible Official sign below will not delay the Approval Order, but will require a separate update to your Operating Permit Application or a request for modification of your Operating Permit, signed by the Responsible Official, in accordance with R307-415-5a through 5e or R307-415-7a through 7i.

**"Based on reasonable inquiry, I certify that the information provided for this Approval Order has been true, accurate and complete and request that this Approval Order be administratively amended to the Operating Permit (Application)."**

Responsible Official \_\_\_\_\_

(Signature & Date)

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**TYPE OF IMPACT AREA**

|   |                       |
|---|-----------------------|
| Attainment Area   | Yes                   |
| NSPS  | Yes                   |
| 40 CFR Part 60, Subpart Da (Fossil-Fuel-Fired Steam Generators for Which Construction is Commenced After September 18, 1978), and Subpart Y (Coal Preparation Plants) |                       |
| NESHAP  | No                    |
| MACT  | No                    |
| Hazardous Air Pollutants (HAPs)   | Yes (from combustion) |
| Hazardous Air Pollutants Major Source<br>(No HAPs involved in modification)   | Yes                   |
| New Major Source  | No                    |
| Major Modification  | No                    |
| PSD Permit  | Yes                   |
| PSD Increment (modeling)  | Yes                   |
| Operating Permit Program  |                       |
| Area Source   | No                    |
| Major   | Yes                   |
| Send to EPA   | Yes                   |
| Comment period  | 30-day                |

**FOR MODIFIED SOURCES**

The Notice of Intent is for a modification to an existing source. The following standards are applicable to this review:

|  |     |
|--|-----|
| NSPS applies to modification?            | No  |
| CO PSD review of entire source required? | Yes |
| NESHAPS applies to modification?         | No  |
| HAPs involved in modification?           | No  |
| TITLE V required for entire source?      | Yes |
| HAPs MAJOR for modification?             | No  |
| NONATT MAJOR for entire source?          | No  |

### Abstract

*Intermountain Power Service Corporation (IPSC) operates the Intermountain Generating Station (IGS) coal fired steam-electric plant, consisting of two 950 MW units approved in the DAQE-049-02), located near Delta in Millard County. IPSC is requesting a modification to their current approval order (AO) DAQE-049-02 to install combustion and NO<sub>x</sub> control system (overfire air) to accommodate the restriction on NO<sub>x</sub> emissions imposed by the Acid Rain Program regulations. In addition, IPSC is proposing:*

- Replacement-in-kind for the Boilers 1 & 2 low-NO<sub>x</sub> burners*
- To replace power supplies and motor drives to induced fans*
- To clarify and specify where surface-heating area was actually to be added in the Boilers 1 & 2*
- Convert minor indoor fugitive emissions to point source outside vented emissions*
- Distributed Control System*

*Projected emission changes from this project are from zero to a potential 7,900 ton decrease from the current NO<sub>x</sub> PTE with concurrent increase of CO from zero to a potential 9,700 tons. Other pollutants emission rates, stack mass flow, stack temperatures, air contaminant types, and concentrations of air contaminants will remain the same. This project represents a major modification under the Prevention of Significant Deterioration (PSD) program since the proposed physical change can result in the significant emission increase for CO.*

*Air quality impact analysis of the CO maximum emission increases was performed and it showed that 1 and 8 hours impacts were well below significant impact levels. Furthermore, potential reduction in the target emissions of NO<sub>x</sub> is expected to improve visibility and expand available NO<sub>x</sub> increments.*

*Millard County is an attainment area of the National Ambient Air Quality Standards (NAAQS) for all pollutants. New Source Performance Standards (NSPS), Subpart Da and Subpart Y apply to this source. Boiler 1 & 2 are also Group 1, Phase II units under the Acid Rain Program. IPSC is a PSD major source of NO<sub>x</sub>, SO<sub>2</sub>, CO, and PM<sub>10</sub>. Title V of the 1990 Clean Air Act applies to this source. The OFA system shall be operated in accordance the current Title V operating permit until that permit is amended. The Title V permit must be modified prior to operation of this modification.*

### Newspaper Notice

A notice of intent for the following project submitted in accordance with §R307-401-1, Utah Administrative Code (UAC), has been received for consideration by the Executive Secretary, Utah Air Quality Board:

Intermountain Power Service Corporation (IPSC), 850 West Brush Wellman Road, Delta, Utah.

Project Location: 850 West Brush Wellman Road Delta, Millard County, Utah

Project Description: IPSC is requesting a modification to their current approval order (AO) DAQE-049-02 to install combustion and NO<sub>x</sub> control system (overfire air) to accommodate the restriction on NO<sub>x</sub> emissions imposed by the Acid Rain Program regulations. In addition, IPSC is proposing:

- Replacement-in-kind for the Boilers 1 & 2 low-NO<sub>x</sub> burners
- To replace power supplies and motor drives to induced fans

- To clarify and specify where surface-heating area was actually to be added in the Boilers 1 & 2
- Convert minor indoor fugitive emissions to point source outside vented emissions
- To upgrade the plant distributed controls system

The proposed emissions increases (in tons per year) will be as follows: PM<sub>10</sub> 0.88 and CO 9702.7.

It has been determined that the conditions of the Utah Administrative Code R307-401-6 and the Federal rules have been met. The Executive Secretary intends to issue an Approval Order after a 30-day public comment period is held. This comment period is being held to receive and evaluate public input on the project proposed by Intermountain Power Service Corporation.

## **I. DESCRIPTION OF PROPOSAL**

IGS is a fossil fuel-fired steam-electric generating station that primarily uses coal as fuel for the production of steam to generate electricity. Both bituminous and sub-bituminous coals are utilized. Fuel oil and used oil are also combusted for start-up, flame stabilization and energy recovery.

IGS is a two-unit facility currently approved to operate at a rated capacity of 950 megawatts (MW). Boiler capacity will be rated at 6.9 million pounds per hour of steam flow at 2,822 psi and 1005°F.

IGS has in place bulk handling equipment for the unloading, transfer, storage, preparation, and delivery of solid and liquid fuel to the boilers. No changes of this equipment are required nor expected. No changes in the usage of other raw materials or bulk chemicals are required nor expected.

### **PROPOSED CHANGES:**

Rectified power drives and motors for induced fan motors need to be replaced due to obsolescence. IPSC has approval to increase surface area to the main boilers, and IPSC is now clarifying the location. IPSC is also requesting approval to install over-fire-airports in each boiler to enhance current operating strategies for controlling combustion and NO<sub>x</sub> emissions. These changes are needed specifically for reliability, performance and/or routine maintenance needs, will not increase approved plant capacity. IPSC is proposing to upgrade its distributed controls system. In addition, IPSC is performing replacement in kind of Boiler #1 & #2 Low-NO<sub>x</sub> burners.

### **BACKGROUND**

On January 11, 2002, the Utah Division of Air Quality (UDAQ) issued to Intermountain Power Service Corporation (IPSC) an approval order (DAQE-049-02) to make certain modifications to the Intermountain Generating Station (IGS). On September 23, 2002, IPSC submitted a Notice of Intent (NOI) to clarify and adjust the scope of those modifications, known as the Dense Pack Uprate Project, as well as receive permitting for other changes. This review is being used to

summarize the Dense Pack Project and certain other changes previously approved by UDAQ (DAQE-049-02).

Approval Order DAQE-049-02 allowed IPSC to make certain changes provided IGS operated those changes as a minor modification pursuant to actual to future actual provisions under Utah's Prevention of Significant Deterioration (PSD) rules. Changes allowed under that Approval Order as described in its original NOI included:

- Increasing heat input to main boilers
- Adding surface area to main boilers
- Replacing each unit high pressure turbine with new technology turbines
- Replacing one relief valve on each main boiler with one safety valve
- Adding wall rings to each scrubber module
- Adding helper cooling towers and cooling system enhancements
- Enhancements to generators, isophase & motor buses, transformers, boiler feed pumps, high pressure lines, control systems, and other similar changes.

**The September 23, 2002 NOI and subsequent requests sought:**

- To clarify where surface area was actually to be added in main boilers
- To replace power supplies and motor drives to induced fans
- Replacement-in-kind for low-NO<sub>x</sub> burners
- To add overfire air ports to main boilers for combustion and NO<sub>x</sub> control.
- To provide outside venting for slurry tank that currently vent within scrubber buildings.
- To upgrade the plant distributed controls system.

Full descriptions of those changes were discussed in IPSC NOI and in subsequent letters, e-mails, and meetings between IPSC and DAQ staff. Additionally, in order to assess how OFA affects both NO<sub>x</sub> and CO emissions, an experimental AO was issued on February 14, 2003 to allow installation and testing of an OFA system on Unit 1 to establish relationship between CO and O<sub>2</sub> and NO<sub>x</sub> control effectiveness with over-fire air.

**PERMIT OPTIONS**

Of particular interest for this NOI is how to treat the permitting for over-fire air (OFA). IPSC initially sought to have OFA permitting as a minor modification under certain PSD provisions. However, the testing of the OFA system is complete, the results showed that CO might increase in major net significant amounts (greater than 100 tons per year) when NO<sub>x</sub> is controlled to low emission rates.

For the dense pack modifications, IPSC chose to modify combustion for NO<sub>x</sub> control during increased heat input, rather than utilize technological add-on controls. Combustion in the boiler was fine-tuned to optimize performance against NO<sub>x</sub> emissions using such methods as burner-out-of-service, excess oxygen control, fuel management, and other boiler operational changes.

Although such practices have been successful, IPSC believes that replacing this combustion

methodology with technical add-on controls would better optimize boiler performance and control of NO<sub>x</sub> emissions.

The use of OFA will allow IPSC to control NO<sub>x</sub> without a significant net increase due to the dense pack modifications. However, IPSC believes it is possible that certain OFA configurations can cause a net significant increase in CO emissions. Therefore, IPSC seeks permitting of OFA as a major modification for CO under PSD.

#### PRODUCTION SUMMARY:

IPSC operate two power generating units, each 950 MWhe, with steam flow of 6.9 million pounds per hour, heat input of 9,225 million Btu per hour, requiring the use of 5.6 million tons of coal each year. See AO #DAQE-049-02 and it's corresponding NOI for details. Nothing with IPSC current NOI is intended to change those production aspects of the previously approved uprate project.

#### EMISSION CHARACTERISTICS:

The composition and physical characteristics of emissions resulting from the proposed modifications are not expected to change with the exception of carbon monoxide (CO), which may increase by a net significant amount. Other pollutant emission rates, chimney mass flow, temperature, air contaminant types, and concentration of air contaminants will remain the same as proposed in the uprate project. The current pollution control devices (PCD) include low-NO<sub>x</sub> burners, fabric filters and wet scrubbers. No increases in PTE for any pollutant except for CO will occur.

Specifically, it is possible for CO emissions to increase as over-fire air (OFA) is used to decrease NO<sub>x</sub> emissions. When NO<sub>x</sub> emissions are fully minimized utilizing OFA, IPP expected that CO emissions could increase from 1989.6 tons per year (as calculated by AP-42- EPA's compilations of emission factors, and verified with testing) to 11,692.3 tons per year (as projected by boiler testing).

The following 30-day average emission rate parameters are provided as required:

| Parameter         | Current<br>Before PCD | Expected<br>After PCD | Potential change after p<br>modification |
|-------------------|-----------------------|-----------------------|--|
| Particulates      | 96,000 lbs/hr         | 50 lbs/hr             | none                                     |
| Nitrogen Oxides   | 0.42 lbs/MMBtu*       | 0.40 lbs/MMBtu        | 0.37 lbs/MMBtu minimum                   |
| Sulfur Dioxide    | 1.8 lbs/MMBtu         | 0.06 lbs/MMBtu        | none                                     |
| Carbon Monoxide   | 0.022 lbs/MMBtu**     | 0.040 lbs/MMBtu       | ***0.143 lbs/MMBtu maximum               |
| Temperature       | 325 F                 | 120 F                 | none                                     |
| Stack Gas Volume  | 130,000,000 scfh      | 130,000,000 scfh      | none                                     |
| VOC               | 1.71 lb/hr            | 1.71 lb/hr            | immeasurable                             |
| Hydrochloric Acid | 0.67 lbs/hr           | 0.02 lbs/hr           | none                                     |
| Hydrofluoric Acid | 0.14 lbs/hr           | 0.004 lbs/hr          | none                                     |

|           |               |                  |      |
|-----------|---------------|------------------|------|
| Antimony  | 0.007 lbs/hr  | 0.000008 lbs/hr  | none |
| Arsenic   | 0.03 lbs/hr   | 0.00006 lbs/hr   | none |
| Beryllium | 0.0009 lbs/hr | 0.0000005 lbs/hr | none |
| Cadmium   | 0.001 lbs/hr  | 0.00001 lbs/hr   | none |
| Chromium  | 0.06 lbs/hr   | 0.0001 lbs/hr    | none |
| Cobalt    | 0.006 lbs/hr  | 0.00001 lbs/hr   | none |
| Lead      | 0.013 lbs/hr  | 0.00003 lbs/hr   | none |
| Manganese | 0.016 lbs/hr  | 0.00005 lbs/hr   | none |
| Mercury   | 0.0001 lbs/hr | 0.00001 lbs/hr   | none |
| Nickel    | 0.009 lbs/hr  | 0.00005 lbs/hr   | none |
| Selenium  | 0.005 lbs/hr  | 0.00065 lbs/hr   | none |

**NOTES:**

\*NO<sub>x</sub> emissions are estimated AFTER low NO<sub>x</sub> combustion.

\*\*Current CO emissions based upon AP-42 factors and testing with OFA:

\*\*\*modified CO emissions based upon testing.

Carbon monoxide (CO) emission rates are provided based upon two different derivations. The current CO rate of 0.022 lbs/MMBtu is based upon AP-42 calculations (this value was also shown to be the same in the testing performed before the PCD). The projected CO rate is based upon testing of overfire air. The increase from a current calculated rate to a projected rate is about 9,700 tons for the plant NO<sub>x</sub> emissions can concurrently decrease up to 7,900 tons from plant PTE.

**Pollution Control Device Description:**

Present pollution control device equipment for combustion for the Unit 1 and 2 boilers includes dual-register low NO<sub>x</sub> burners, baghouse type fabric filters for particulate removal, and flue gas desulfurization scrubbers. Control equipment for the handling and transfer of solid material include dust collection filters.

**Pollution Control Device Upgrade:**

The project includes the addition of overfire air (OFA) ports and replacement or repair of dual register low NO<sub>x</sub> burners.

**Description of the Overfire Air (OFA) System and Control Devices.**

Overfire air is needed, in part, to accommodate the restriction on NO<sub>x</sub> emissions imposed by Acid Rain regulations that were promulgated based upon the Clean Air Act Amendments of 1990. Specifically, in 2007, Acid Rain requirements impose a 0.46 lb/MMBtu annual cap for NO<sub>x</sub> emissions on IPP. Since an early election was filed for IPP, this new limit was delayed. Current forecasts of coal quality indicate that without OFA, the new Acid Rain limit could be difficult to attain. A multiport overfire air system will be added to ensure stable operation in accordance with specified emissions limits. The OFA system will redirect approximately 10-15 percent of total combustion air to a staged system of ports located directly above the top row of

burners.

The OFA system at the Intermountain Generating Station (IGS) is being provided by Babcock Power, Inc. (BPI). It consists of one row of OFA ports located on the elevation immediately above the top burner levels on both the front (south) and rear (north) sides of the boiler. Each row consists of eight, identical, OFA ports with one port located over each of the six burner columns (column ports) and one port located on each end of the OFA rows near the side walls of the boiler (wing ports).

Air to the OFA system is provided by the Secondary Air (SA) system. A feeder duct extends from each SA header duct to the corresponding OFA header through which secondary air is admitted to the OFA headers. Each OFA feeder duct includes isolation dampers operated by Jordan rotary electrical drives.

OFA airflow to the boiler is admitted and controlled through the OFA port dampers. Each OFA port is partitioned into separate 1/3 and 2/3 sections. Airflow, through each set of OFA ports, is controlled by port dampers located in each partition. The four, 1/3 port dampers for an OFA row half are connected or ganged together for simultaneous operation by a Jordan rotary electrical drive. The same configuration is implemented for the 2/3 port damper sets. This creates a total of four, 1/3 port dampers/drives and four, 2/3 port dampers/drives for over-air flow control to the boiler.

Control and monitoring of all OFA damper drives is done by the IGS combustion control system. Additionally, an array of three Air Monitor Corporation VOLU-probes and thermocouples measures OFA mass flow through each of the four feeder ducts. Control signals operate all port dampers simultaneously; independent damper control is not available.

#### **Control Strategy Description**

More detailed information is in the documentation provided by Babcock Power Interface included in the "Report on Good Combustion Practices".

OFA is most effective controlling NO<sub>x</sub> formation at unit loads above 60% of the rated load of 950 MW. When utilized at the 60% load point and above, OFA flow will be accomplished by the combination of opening OFA feeder and port dampers and decreasing the combustion air damper positions, so as to maintain target total SA flow based on unit load.

The OFA port and feeder duct damper groups have modulating capability and can be operated either fully open, fully closed, or throttled to positions in-between. (Open position can be biased to achieve balanced O<sub>2</sub> distribution across the burner front). SA airflow to the OFA system is attained by simultaneously decreasing the openings of all the combustion air dampers feeding each of the burner elevations that are in operation. This decrease is superimposed on the existing automatic control biasing of each elevation combustion air in accordance with pulverizer loading.

This SA damper control is additive to the existing bias required to change burner airflow in



proportion to the individual pulverizer load. The action of the sum of both biases will result in less secondary air directly to the burners, as OFA is being introduced, but the relative secondary air distribution between burner elevations will remain unchanged.

The OFA port relative open area sizes, 1/3 and 2/3, are calculated to provide the correct velocity of the OFA to attain the proper penetration of the OFA into the combustion region of the furnace above the burners. All ports of a given kind, 1/3 or 2/3, will open or close following a program designed to open the correct area to roughly produce the proper penetration velocity as the OFA air flow rate changes with boiler load. OFA operation will include the following configurations:

All 1/3 and 2/3 ports closed  
1/3 ports open, 2/3 ports closed  
1/3 ports closed, 2/3 ports throttled  
1/3 ports closed, 2/3 ports open

#### **Target Operating Parameters for OFA Design**

The OFA modifications shall provide for a continuous boiler rating of 6,900,000-lbs/hr output at 1005°F superheat and 1005°F reheat temperature under normal operating conditions. These modifications shall include the design, fabrication and installation on both IGS Units 1 & 2 for an overfire air system capable of providing a reduction in NO<sub>x</sub> emissions of 15% and consistent NO<sub>x</sub> emissions of less than 0.40 lbs/MMBtu under all operating modes.

Of particular interest to IPSC were the performance parameters associated with operation at 950 Megawatts gross generation (6.75 MMlbs/hr steam flow). These include:

- a. Total NO<sub>x</sub> output of 0.40 lbs/MMBtu or less up to an overall reduction of 15%. Current maximum average of 0.461 lbs/MMBtu.
- b. Superheat and reheat temperatures as well as NO<sub>x</sub> emissions must remain within acceptable ranges.
- b. Minimal impact on average unburned carbon (LOIs) and carbon monoxide (CO) concentrations within the boiler.

NOTE: These are target parameters only for purposes of OFA design and performance evaluation, and in no way IPSC intended to limit boiler operation in any way.

#### **EMISSION POINT:**

The present emission point for the IGS boilers is a lined chimney that discharges at 712 feet above ground level (5,386 feet above sea level). The chimney location is 39° 39' 39" longitude, 112° 34' 46" latitude.

#### **SAMPLING/MONITORING:**

Emissions from boiler combustion are continuously sampled and monitored at the chimney for nitrogen oxides, sulfur oxides, carbon dioxide, and volumetric flow. Opacity is measured at the fabric filter outlet. Other parameters recorded include heat input and production level (megawatt load). Monitoring will remain unchanged. Other emissions not directly monitored are calculated using engineering judgments, emission factors, and fuel analyses.

#### **OPERATING SCHEDULE:**

Operation at IGS is 24 hours per day, seven days per week.

#### **MODIFICATION SPECIFICATIONS and CONSTRUCTION SCHEDULE:**

##### **a. Induced Fan Drive Power Supply Obsolescence & Replacement**

There are four induced draft (ID) fans for each generator at the Intermountain Generating Station. The fans are centrifugal airfoil, double width, double inlet design driven by synchronous motors through variable frequency drives. The flow modeling has shown the best approach to correcting our obsolescence problem may be to replace our current power drives with new induced pulse width modulation technology. Such a change would require motor replacements. The existing variable frequency drives are of 1980 vintage, no longer manufactured, require increasing maintenance, certain critical repair parts are no longer available, and frequently fail, although such failures do not currently impact station operation due to fan redundancy. The variable frequency drives are scheduled for replacement beginning in 2004. Replacement of the variable frequency drive systems will not include modifications of the existing fans and no change beyond approved capacity would result from the possible drive and motor horsepower change out. We are therefore requesting approval accordingly.

##### **b. Changes to Approved Boiler Modifications**

Previously approved but uncompleted boiler modifications included the addition of preheat steam tubes to the convective pass of each boiler. Due to latest modeling and operational data, this NOI proposes to change those modifications to the radiant section of the boiler, which will include the addition of platen superheater surface. The 36-platen superheater pendants, in each boiler, are scheduled to be lengthened by approximately 8 feet from their present approximate 40-foot length. The purpose of these changes was for better combustion control. These proposed changes are still on track for Unit 1 and Unit 2 in March 2004, meeting the construction schedule originally set forth under DAQE-049-02.

##### **c. Low NO<sub>x</sub> Burner Maintenance & Replacement**

IPSC proposes to replace the existing burners as needed in future years. Burners have not met their design life and need to be replaced or rebuilt. The replacement or rebuild of the present low NO<sub>x</sub> burners is proposed as replacement-in-kind, as IPSC does not propose to increase heat input through the new burners from what currently exist.

The current burners have already been shown in different tests to accommodate heat input rates of the current uprate modification (9,225 MMBtu/hr). Tests in April of 2002, demonstrated maximum heat input per existing burner (B&W with 58" throat) to be 248 MMBtu per hour. New low NO<sub>x</sub> burners (Advanced Burner Technologies, Opti-Flow with 51" throat and will be limited with maximum heat input per burner at up to 248 MMBtu per hour at the same NO<sub>x</sub> control levels to qualify as replacement-in-kind. Additionally, the maximum burner heat input level is limited with existing mills (B&W ModelMPS89). Burner maintenance and repair for Unit 1 and burner replacement for Unit 2 will begin in 2004 and continue through 2008 in a multi-staged process.

**d. OFA Ports**

A multiport OFA system will be added to ensure stable operation in accordance with specified emissions limits. IPSC currently uses a combustion tuning methodology for NO<sub>x</sub> control that they find is costly and somewhat haphazard. OFA air is also needed, in part, to accommodate the restriction on NO<sub>x</sub> emissions imposed by Acid Rain regulations that were promulgated based upon the Clean Air Act Amendments of 1990. Specifically, in 2007 Acid Rain requirements impose a 0.46 lb/MMBtu annual cap for NO<sub>x</sub> emissions on IPP. Since an early election was filed for IPP, this new limit was delayed. Current forecasts of coal quality indicate that without OFA, the new Acid Rain limit could be difficult to attain.

The OFA system will redirect approximately 10 to 15 percent of total combustion air to a staged system of ports located directly above the top row of burners. When OFA is utilized to minimize NO<sub>x</sub> emissions as much as possible, CO emissions may increase by a net significant amount.

A full description of the OFA system and its operation has already been filed. In fact, IPSC has installed and tested an OFA system on Unit One as allowed by an experimental approval order. The results of the test confirmed potential CO increases with OFA system.

**e Distributed Control System**

IPSC had proposed replacement and upgrade of the distributed control system at IGS in the April 2001 NOI. However, AO #DAQE-049-02 did not specifically identify the DCS replacement, except for the description in the AO abstract as "other similar changes." For clarity, IPSC wishes to have the DAQ specifically identify the DCS project in the AO, and treat this NOI as such request. Certain control systems will be upgraded as an integral part of the uprate modification (i.e., new turbine, boiler modifications, OFA system) and are considered part of those modifications. However, IPSC is proposing to upgrade all corresponding operating control systems as well. The Intermountain Generating Station is controlled by several subordinate systems. These systems include a coordinated control system, a burner management system, a combustion control system, a turbine electro-hydraulic control system, a turbine supervisory system as well as several plant data acquisition and status display systems. Components within these systems are becoming increasingly hard to obtain from either primary or secondary manufacturers. Although there have been no system failures that have caused forced outages, these control systems are now causing reliability concerns due to the unavailability of key

hardware.

The existing control systems are scheduled to be replaced beginning in the 2004 spring outage. The various control systems will be replaced with a centralized, distributed control system in a phased approach over a several year period to reduce the impact on generation capability. The current schedule shows this project being completed in the spring of 2007.

**f. New Point Source Venting**

IPSC is proposing to vent minor indoor source fugitive emissions to vented point source emissions.

There are six tanks in each the two scrubber buildings. Four are in operation at any given time for each unit to control sulfur and acid gas emissions. A diagram indicating proposed venting, and a worksheet indicating worst-case emissions was submitted as part of the NOI. We do not believe that particulates are a significant part of venting, but we have included those calculations based upon evaporation rates. Emissions are characterized worst case as follows:

|   |                                     |
|---|-------------------------------------|
| Estimated Vent Flow Rate                | 2500cfm                             |
| Emission Temperature                    | 51° C                               |
| Vent Particulate Emission Rate          | 0.11 tons/yr                        |
| Number of Operating Vents               | 8 (out of 12)                       |
| Total Emission Rate (PM <sub>10</sub> ) | 0.88 tons/yr                        |
| Stack Vent Elevation                    | 4825 ft (149 ft above ground level) |

**Applicability Determinations**

**OFA**

The installation of OFA to the Units One & Two boilers can be expected to cause a decrease in NO<sub>x</sub> with a concomitant increase in CO. This follows a sliding relationship; i.e., if NO<sub>x</sub> levels are maintained, no CO increase can result. If NO<sub>x</sub> is minimized to the greatest extent possible, CO may rise accordingly. IPSC predicts that normal operation will show a slight decrease in NO<sub>x</sub> with the use of overfire air, resulting in a small increase in CO.

IPSC in its NOI did not propose any requirement that IPSC must operate the OFA and Low-NO<sub>x</sub> burners to fully minimize NO<sub>x</sub>. IPSC's intent in adding further NO<sub>x</sub> controls is to balance combustion performance with environmental control. IPP intends to continue to operate in such a manner that maximizes performance, yet still meets environmental limits as mandated by regulation and permit. This means that NO<sub>x</sub> will be controlled to meet short-term thirty-day rolling average limits, as well as the annual WEPCO requirements outlined in the AO.

**New Source Performance Standards.**

IGS operates as a New Source Performance Standard (NSPS) power plant, regulated under Title 40 of the Code of Federal Regulations, Part 60, Subpart Da. The proposed changes do not trigger NSPS applicability. "Modification" is defined at 40 CFR 60.14 to include any change in

operation of a source that increases the maximum hourly emissions of a Part 60 regulated pollutant above the maximum achievable during the previous five years. (See 40 CFR 60.14(h)). Even though the use of OFA to enhance combustion and reduce NO<sub>x</sub> can increase carbon monoxide (CO), CO is not a regulated pollutant under NSPS Subpart Da, which is applicable to IGS.

#### **Prevention of Significant Deterioration.**

IGS was constructed under Prevention of Significant Deterioration (PSD) permits, and with the exception of possible CO increases, none of the changes proposed are a major modification for PSD purposes. Based upon boiler combustion performance modeling and tests, CO emissions are expected to increase by a net significant amount (greater than 100 tons per year). Those projected CO increases have been modeled for possible air impacts and have been shown they do not cause or contribute to a violation of a NAAQS, PSD increment, or adverse Class I impact. Those modeling results have already been submitted to UDAQ.

#### **Modeling**

CO modeling was performed for the total potential emission of CO to evaluate if increases do not cause or contribute to a violation of a NAAQS, PSD increment, or adverse Class I impact. For the worst case 1 hour CO short term emission rate of 11,439 lbs/hr, ISC modeling shows results of 941.5 ug/m<sup>3</sup>. For the 8 hour CO short term emission rate of 5,719.5 lbs/hr, ISC modeling shows impact results of 119.8 ug/m<sup>3</sup>. This is well below the modeling significant levels of 2000 and 500 ug/m<sup>3</sup>, respectively, confirming no adverse contribution or violation.

#### **Title V Permit**

IGS operates under a Title V permit (#2700010001). IPSC intends to continue to operate in full compliance with that permit and applicable requirements. -

The changes proposed herein will affect only one condition of the current Title V permit. Condition II.B.1.i limits CO emissions on an annual basis. Since maximizing NO<sub>x</sub> control efficiency can cause CO emissions to exceed this limit, IPSC requests that this condition be revised accordingly.

## **II. EMISSION SUMMARY**

The emissions from Intermountain Generating Station will be as follows:

| <u>Pollutant</u>   | <u>Current Emissions<br/>tons/year</u> | <u>Emission Increases<br/>tons/year</u> | <u>Total Emissions<br/>tons/year</u> |
|--|--|---|--------------------------------------|
| PM <sub>10</sub>   | 3,286.7                                |   | 3,286.7                              |
| (Can we subsume this into our current PTE? The emissions are not new; just already present as fugitive.) |  |   |                                      |
| SO <sub>2</sub>  | 11,332.3                               | 0.00                                    | 11,332.3                             |
| NO <sub>x</sub>  | 37,868.2                               | 0.00                                    | 37,868.2                             |

|                    |         |        |          |
|--------------------|---------|--------|----------|
| CO                 | 1989.6  | 9702.7 | 11,692.3 |
| VOC                | 63.91   | 0.00   | 0.00     |
| HAPs               |         |        |          |
| Lead               | 0.39168 | 0.00   | 0.39168  |
| Berillium          | 0.00892 | 0.00   | 0.00892  |
| Fluorides (HF)     | 16.8    | 0.00   | 16.8     |
| Sulfuric Acid      | 8.8     | 0.00   | 8.8      |
| Mercury            | 0.00    | 0.00   | 0.00     |
| Total HAPs         | 0.00    | 0.00   | 82.67    |
| Other NON-VOC HAPs | 93.2    | 0.00   | 93.2     |

### III. BEST AVAILABLE CONTROL TECHNOLOGY (BACT)

#### Good Combustion Practice

Since fuel utilization and combustion efficiency suffer in attempts to minimize NO<sub>x</sub> generation in the boiler, CO can rise due to incomplete or poor combustion. There are no add-on controls specific to CO technologically, nor are they commercially available in any form for utility steam generators. As a matter of practice, BACT for CO is considered to be Good Combustion Practice.

Good combustion practice (GCP) is defined as system design, operation, and maintenance techniques, which can increase combustion efficiency. The GCP control strategy includes collectively applying a number of combustion conditions to achieve three broad goals:

- (1) Maximize fuel utilization and boiler efficiency;
- (2) Minimize byproducts of poor combustion (CO) and
- (3) Minimize creation of combustion related pollutants (NO<sub>x</sub>).

The emphasis in an effective good combustion practice lies in the design of the combustion system. There are several specific measurable parameters that compose a set of combustion indicators that can be related directly or indirectly to the design of the GCP components. These combustion parameters are:

- CO levels in the flue gas;
- Loss of Ignition of carbon in the ash;
- NO<sub>x</sub> levels in the flue gas
- Excess O<sub>2</sub> in the combustion air; and
- Heat Rate (i.e., plant efficiency - heat input vs. load production).

Good combustion is essentially a balance of the GCP components, which by the nature of the combustion process are antagonistic. High fuel utilization and boiler performance increases NO<sub>x</sub> creation. Minimizing NO<sub>x</sub> through combustion controls increases CO and LOI, and decreases efficiency. GCP design balances these effects to optimize each component. CO is a good indicator of combustion efficiency, which when measured before and after modifications to a combustion process, can verify GCP design.

The ability to maintain low CO and NO<sub>x</sub> concentrations in flue gases is dependent on combustion design features such as those found in retrofit OFA ports. Once the design has been demonstrated to be GCP, GCP is further employed in operating and maintenance practices. Since CO is minimized as an inherent component to maximizing efficiency and lowering operating costs, there exists a natural incentive towards GCP in OFA operation and maintenance. Since OFA has been tested and emissions of CO can be correlated to other operating parameters, GCP therefore can be demonstrated through the application of those correlation curves to actual operation.

#### **Best Available Control Technology (BACT).**

IGS was constructed under a PSD permit which required BACT. Since the CO emissions increases may trigger a major PSD modification, a Top Down CO BACT analysis was performed.

#### **Top-Down BACT Process**

EPA has developed a process for conducting BACT analyses. This method is referred to as the "top-down" method. The steps are:

- Step 1 – Identify All Control Technologies
- Step 2 – Eliminate Technically Infeasible Options
- Step 3 – Rank Remaining Control Technologies by Control Effectiveness
- Step 4 – Evaluate Most Effective Controls and Document Results
- Step 5 – Select BACT

Each of these steps has been conducted for CO and is described below.

Potential control technologies for CO were identified from a number of sources including the EPA RBLC database, control technology vendors, technical journals and web sites, and other recently issued permits

#### **CO Analysis**

The BACT analysis for CO is presented below.

##### **Step 1 – Identify All Control Technologies**

Only two control technologies have been identified for control of CO on coal-fired boilers:

Catalytic oxidation

Combustion controls

Catalytic oxidation is a post-combustion control device that would be applied to the combustion system exhaust, while combustion controls are part of the combustion system design.

##### **Step 2 – Eliminate Technically Infeasible Options**

Catalytic oxidation has been the control alternative used to obtain the most stringent control level

for CO emitting from primarily combustion turbines firing natural gas. This alternative, however, has never been applied to a PC-fired unit so this technology has not been demonstrated in practice in this application.

For sulfur containing fuels, such as coal, an oxidation catalyst will convert  $\text{SO}_2$  to  $\text{SO}_3$  and therefore this conversion would result in unacceptable levels of corrosion to the flue gas system. Generally, oxidation catalysts are designed for a maximum particulate loading of 50 milligrams per cubic meter ( $\text{mg}/\text{m}^3$ ). The IPP boilers have a particulate loading upstream of the fabric filter well above this value. In addition, trace elements present in coal, in particular chlorine, are poisonous to oxidation catalysts. There are no catalysts developed that have or can be applied to PC-fired boilers due to the high levels of PM and trace elements present in the flue gas. Although the catalyst could be installed downstream of the fabric filter where the concentration of PM in the flue gas is much lower than at the outlet of the boiler, the flue gas temperature at that point will be approximately 300°F. This is well below the minimum temperature required (600°F) for operation of oxidation catalyst. The flue gas would have to be reheated, resulting in significant unfavorable energy and economic impacts.

For these reasons, as well as the generally low levels of CO in PC-fired units, no PC-fired boilers have been equipped with oxidation catalysts. Use of an oxidation catalyst system in the PC-fired boiler is thus considered technically infeasible. Thus, this alternative cannot be considered to represent BACT for control of CO.

#### Step 3 – Rank Remaining Control Technologies by Control Effectiveness

Based on the Step 2 analysis, combustion control is the only remaining technology for this application.

#### Step 4 – Evaluate Most Effective Controls and Document Results

There are no environmental or energy costs associated with combustion control.

#### Step 5 – Select BACT

Based on the above analysis, a Good Combustion Practice (GCP) for CO is selected as BACT. IPSC has provided a detailed discussion on what GCP entails for boiler operation utilizing OFA.

With regard to CO, BACT can only be provided through the application of good combustion practices (GCP), which is already in place, and is intimately related to best boiler performance, a strong business incentive. No other technological controls are available for CO in coal-fired boilers.

IPSC has provided a proposal on how GCP can be implemented, and the testing of OFA will help determine the parameters by which GCP can be verified.

#### Permitting



IPSC proposed that to verify GCP in the OFA design, boiler O<sub>2</sub> be measured during OFA operation. Testing at Unit 1 has shown that excess boiler O<sub>2</sub> is the single best indicator of CO emissions at various OFA configurations. CO can be directly calculated accordingly. CO results were reported to the Utah DAQ accordingly to confirm GCP. The other parameters will be monitored for quality assurance and performance of OFA operation, but not reported. IPSC proposes to maintain for inspection relevant records of operating and maintenance data to reflect continuing GCP utilizing data sources presently and readily available.

#### **IV. APPLICABILITY OF FEDERAL REGULATIONS AND UTAH ADMINISTRATIVE CODES (UAC)**

The Notice of Intent submitted is for an existing source. At the time of this review the Utah Administrative Code Rules 307 (UAC R307) and federal regulations have been examined to determine their applicability to this Notice of Intent. The following rules have been specifically addressed.

1. R307-101-2, Major Modification - means any physical change in or change in the method of operation of a major source that would result in a significant net emissions increase of any pollutant.
2. R307-107, UAC - Unavoidable breakdown reporting requirements
3. R307-150 Series, UAC - Inventories, Testing and Monitoring. These rules cover emission inventory reporting requirements and require the owner or operator of sources of air pollution to submit an emissions inventory report:  
  
R307-150. Emission Inventories  
R307-155. Hazardous Air Pollutant  
R307-158. Emission Statement Inventory.
4. R307-201-1(2), UAC - 20% maximum opacity limitation at all emission points. Visible emissions from installations constructed after April 25, 1971, except internal combustion engines, or any incinerator shall be of a shade or density no darker than 20% opacity, except as otherwise provided in these regulations.
5. R307-201-1(9), UAC - Opacity Observation.
6. R307-203-1(1), UAC - Commercial and Industrial Sources. Any coal, oil, or mixture thereof, burned in any fuel burning or process installation not covered by New Source Performance Standards for sulfur emissions shall contain no more than 1.0 pound sulfur per million gross Btu heat input for any mixture of coal nor .85 pounds sulfur per million gross Btu heat input for any oil.
7. R307-205 (UAC) - Emission Standards: Fugitive Emissions and Fugitive Dust.

8. R307-325-1(1) R307-325 applies to all sources in R307-326 through 341, major sources as defined and outlined in section 182 of the Clean Air Act and non-major sources located in Davis and Salt Lake Counties and in any non-attainment area for ozone as defined in the State Implementation Plan.
9. R307-401-10(1), UAC - All sources excluding non-commercial residential dwellings shall install oxides of nitrogen control/low oxides of nitrogen burners or controls resulting from application of an equivalent technology, as determined by the Executive Secretary, whenever existing fuel combustion burners are replaced, unless such replacement is not physically practical or cost effective. The request for an exemption shall be presented to the Executive Secretary for review and approval.
10. R307-403-3, UAC - Every major new source or major modification must be reviewed by the Executive Secretary to determine if a source will cause or contribute to a violation of the NAAQS.
11. R307-405, UAC - Permits: Prevention of Significant Deterioration of Air Quality (PSD)
  - 405-1. Definitions
  - 405-2. Area Designations
  - 405-3. Area Redesignation
  - 405-4. Increments and Ceilings
  - 405-5. Baseline Concentration and Date
  - 405-6. PSD Areas - New Sources and Modifications
  - 405-7. Increment Violations
  - 405-8. Banking of Emission Offset Credit in PSD Areas
12. – R307-406, UAC – Visibility
  - 406-1.(1) The Executive Secretary shall review any new major source or major modification proposed in either an attainment area or area of non-attainment area for the impact of its emissions on visibility in any mandatory Class I area.
13. R307-410, UAC - Permits: Emissions Impact Analysis (Air Quality Modeling)
14. R307-413, UAC - Permits: Exemptions and Special Provisions
  - 413-1. Definitions and General Requirements
  - 413-2. Small Source Exemptions - De minimis Emissions
  - 413-3. Flexibility Changes
  - 413-4. Other Exemptions
  - 413-5. Replacement-in-Kind Equipment
  - 413-6. Reduction of Air Contaminants
  - 413-7. Exemption from Notice of Intent Requirements for Used Oil Fuel Burned for Energy Recovery
  - 413-8. De minimis Emissions From Air Strippers and Soil Venting Projects
  - 413-9. De minimis Emissions From Soil Aeration Projects.

15. R307-420, UAC - Permits: Ozone Offset Requirements in Davis and Salt Lake Counties.
16. 40 CFR, Part 50 - National Ambient Air Quality Standards (NAAQS). The following areas are Non-attainment areas:
  - PM<sub>10</sub> Salt Lake and Utah Counties, and the city of Ogden
  - SO<sub>2</sub> Salt Lake County and The Oquirrh Mountains above 5,600 feet in Eastern Tooele County
  - CO Provo

The following areas are Maintenance Areas:

  - Ozone Salt Lake and Davis Counties
  - CO Ogden and Salt Lake City
17. 40 CFR 60.15, Definition of Reconstruction - the replacement of components of an existing facility to such an extent that:
  - A. The fixed capital cost of the new components exceeds 50% of the fixed capital cost that would be required to construct a comparable entirely new facility and
  - B. It is technologically and economically feasible to meet the applicable standards set forth in this part.

**V. RECOMMENDED APPROVAL ORDER CONDITIONS****General Conditions:**

1. This Approval Order (AO) applies to the following company:

Intermountain Power Service Corporation  
850 West Brush Wellman Road  
Delta, Utah 84624  
Phone Number: (435) 864-4414  
Fax Number: (435) 864-6670

The equipment listed below in this AO shall be operated at the following location:

**PLANT LOCATION:**

850 West Brush Wellman Road, Delta, Millard County, Utah

Universal Transverse Mercator (UTM) Coordinate System: datum NAD27  
4,374.4 kilometers Northing, 364.2 kilometers Easting, Zone 12

2. All definitions, terms, abbreviations, and references used in this AO conform to those used in the Utah Administrative Code (UAC) Rule 307 (R307) and Title 40 of the Code of Federal Regulations (40 CFR). Unless noted otherwise, references cited in these AO conditions refer to those rules.
3. The limits set forth in this AO shall not be exceeded without prior approval in accordance with R307-401.
4. Modifications to the equipment or processes approved by this AO that could affect the emissions covered by this AO must be reviewed and approved in accordance with R307-401-1.
5. All records referenced in this AO or in applicable NSPS and/or NESHAP and/or MACT standards, which are required to be kept by the owner/operator, shall be made available to the Executive Secretary or Executive Secretary's representative upon request, and the records shall include the five-year period prior to the date of the request. Records shall be kept for the following minimum periods:
  - A. Emission inventories Five years from the due date of each emission statement or until the next inventory is due, whichever is longer.
  - B. All other records Two years

6. Intermountain Power Service Corporation (IPSC) shall install overfire air system on Boiler #1 and Boiler #2, perform replacement in kind of the Boiler #1 and Boiler #2 Low-NO<sub>x</sub> burners (where needed) and shall conduct its operations of the Intermountain Generating Station (IGS) coal fired electric steam plant in accordance with the terms and conditions of this AO, which was written pursuant to IPSC's Notice of Intent submitted to the Division of Air Quality (DAQ) on March 24, 2003 and additional information submitted to the DAQ September 23, 2002, November 14, 2002, November, January 23, 2003, September 25, 2003, November 3, 2003, November 10, 2003, and November 19, 2003.
7. This AO shall replace the AO (DAQE-049-02) dated January 11, 2002.
8. The approved installations shall consist of the following equipment or equivalent\*:
  - A. Unit #1 Coal Fired Boiler (Subject to NSPS, Subpart Da) equipped with Low NO<sub>x</sub> burners with maximum heat input of 248 MMBtu/hr per each burner.  
Rating - 9,225 x 10<sup>6</sup> Btu/hr (MMBtu/hr)
  - B. Unit #2 Coal Fired Boiler (Subject to NSPS, Subpart Da) equipped with Low NO<sub>x</sub> burners with maximum heat input of 248 MMBtu/hr per each burner  
Rating - 9,225 MMBtu/hr
  - C. Coal railcar unloading dust collector 1A
  - D. Coal railcar unloading dust collector 1B
  - E. Coal railcar unloading dust collector 1C
  - F. Coal railcar unloading dust collector 1D
  - G. Coal truck unloading dust collector 2
  - H. Coal reserve reclaim dust collector 3
  - I. Coal transfer building #1 dust collector 4
  - J. Coal transfer building #2 dust collector 5
  - K. Coal transfer building #4 dust collector 6
  - L. Coal crusher building dust collector 11
  - M. U1 Generation building coal dust collector 13A
  - N. U1 Generation building coal dust collector 13B
  - O. U2 Generation building coal dust collector 14A
  - P. U2 Generation building coal dust collector 14B
  - Q. Coal pile-active and reserve
  - R. Coal Stackout
  - S. Fuel oil tank 1A  
Capacity - 675,000 gallons
  - T. Fuel oil tank 1B  
Capacity - 675,000 gallons
  - U. Limestone unloading dust collector 1A
  - V. Limestone unloading dust collector 1B
  - W. Limestone transfer dust collector 1
  - X. Limestone reclaim dust collector 2
  - Y. Limestone silo bin vent filter

|      |  |                                    |
|------|--|------------------------------------|
| Z.   | Limestone crusher dust collector 3   |                                    |
| AA.  | Limestone preparation dust collector 4   |                                    |
| BB.  | Limestone storage pile   |                                    |
| CC.  | Lime silo dust collector 1   |                                    |
| DD.  | Lime hopper dust collector 2   |                                    |
| EE.  | Soda ash silo dust collector 3   |                                    |
| FF.  | Soda ash hopper dust collector 4   |                                    |
| GG.  | Fly ash silo bin vent filter 1A  |                                    |
| HH.  | Fly ash silo bin vent filter 1B  |                                    |
| II.  | Combustion byproducts stackout & stockpile   |                                    |
| JJ.  | Combustion byproducts landfill   |                                    |
| KK.  | Unit 1 cooling tower 1A  |                                    |
| LL.  | Unit 1 cooling tower 1B  |                                    |
| MM.  | Unit 2 cooling tower 1A  |                                    |
| NN.  | Unit 2 cooling tower 1B  |                                    |
| OO.  | Coal sample preparation building dust collector  |                                    |
| PP.  | Sandblast facility dust collector  |                                    |
| QQ.  | U1 Generation building vacuum cleaning dust collector  |                                    |
| RR.  | U2 Generation building vacuum cleaning dust collector  |                                    |
| SS.  | U1 Fabric filter vacuum cleaning dust collector  |                                    |
| TT.  | U2 Fabric filter vacuum cleaning dust collector  |                                    |
| UU.  | GSB vacuum cleaning dust collector   |                                    |
| VV.  | Guzzler truck dust collector   |                                    |
| WW.  | Emergency diesel generators  |                                    |
|      | 1A, rated at -   | 4,000 Hp                           |
|      | 1B, rated at -   | 4,000 Hp                           |
|      | 1C, rated at -   | 4,000 Hp                           |
| XX.  | Solvent washers  |                                    |
| YY.  | Diesel driven fire pump rated at 290 Hp 1B   |                                    |
| ZZ.  | Diesel driven fire pump rated at 290 Hp 1C   |                                    |
| AAA. | Auxiliary boiler 1A (not subject to NSPS)  |                                    |
|      | Rating -   | 166 MMBtu/hr                       |
| BBB. | Auxiliary boiler 1B (not subject to NSPS)  |                                    |
|      | Rating -   | 166 MMBtu/hr                       |
| CCC. | Coal Conveyors   |                                    |
| DDD. | Paint booth/shops  |                                    |
| EEE. | Engine driven equipment including compressors, generators, hydraulic pumps and diesel fire pumps |                                    |
| FFF. | Bulb recycling crusher   |                                    |
| GGG. | Laboratory fume hoods  |                                    |
| HHH. | Gasoline tank  |                                    |
|      | Capacity -   | 500 gallons                        |
| III. | Diesel tank  |                                    |
|      | Capacity -   | 10,000 gallons                     |
| JJJ. | Diesel day tanks   |                                    |
|      | Capacity -   | not exceeding 560 gallons per tank |

- KKK. Mobile oil storage tanks
  - Capacity - not exceeding 12,000 gallons per tank
- LLL. Turbine lube oil units
  - Capacity - not exceeding 40,000 gallons per unit
- MMM. Underground storage diesel tank
  - Capacity - 20,000 gallons
- NNN. Underground storage gasoline tank
  - Capacity - 6,000 gallons
- OOO. Used oil tank
  - Capacity - 10,000 gallons
- PPP. Class III Industrial Waste Landfill
- QQQ. Paved haul roads
- RRR. Unpaved Haul roads (This would match Title V, which differentiates between paved and unpaved requirements.)
- SSS. Coal truck unloading grating
- TTT. Two Helper cooling towers
- UUU. Boiler #1 and Boiler #2 over-fire air-ports, 16 per each boiler
- \* Equivalency shall be determined by the Executive Secretary.
- \* Equivalency shall be determined by the Executive Secretary.

\*\* This equipment is listed for informational purposes only. There are no emissions from this equipment.

9. Intermountain Power Service Corporation shall notify the Executive Secretary in writing when the installation of the equipment listed in Condition #8.A., B. and UUU has been completed and is operational, as an initial compliance inspection is required. To insure proper credit when notifying the Executive Secretary, send your correspondence to the Executive Secretary, attn: Compliance Section.

If construction and/or installation has not been completed within eighteen months from the date of this AO, the Executive Secretary shall be notified in writing on the status of the construction and/or installation. At that time, the Executive Secretary shall require documentation of the continuous construction and/or installation of the operation. If continuous construction and/or installation can not be demonstrated, the Executive Secretary may revoke the AO in accordance with R307-401-11.

#### **Limitations and Tests Procedures**

10. Except for start-up, shut-down, planned/maintenance outage, or malfunction, emissions to the atmosphere at all times from the indicated emission points shall not exceed the following rates and concentrations:

#### **A. Each Main Boiler Stack**

| <u>Pollutant</u> | <u>lb/ 10<sup>6</sup> Btu heat input</u> |  |
|------------------|--|--|
| PM <sub>10</sub> | 0.0184 *                                 | lb/ 10 <sup>6</sup> Btu heat input   |
| SO <sub>2</sub>  | 0.138 **                                 | lb/ 10 <sup>6</sup> Btu heat input based on 30-day rolling-average<br>10.0 % of the potential combustion concentration |
| NO <sub>x</sub>  | 0.461**                                  | lb/ 10 <sup>6</sup> Btu heat input based on 30-day rolling-average   |

1B. Testing Status (To be applied above)

\* Test once a year. The Executive Secretary may require testing at any time.

\*\*Compliance for NO<sub>x</sub> and SO<sub>2</sub> emissions shall be demonstrated through use of a continuous emissions monitoring system as outlined in Condition 24.

B. Dust Collectors

| <u>Pollutant/Source</u>        | <u>Differential pressure range across the dust collector</u><br>(Inches of water gage) |
|--------------------------------|--|
| PM <sub>10</sub>               |  |
| Rail car unloading (4 units)   | 0.5 to 12*   |
| Transfer building one          | 0.5 to 12*   |
| Unit one 13A                   | 0.5 to 12*   |
| Transfer building two          | 0.5 to 12*   |
| Transfer building four         | 0.5 to 12*   |
| Crusher building one           | 0.5 to 12*   |
| Unit one 13B                   | 0.5 to 12*   |
| Unit two 14A                   | 0.5 to 12*   |
| Unit two 14B                   | 0.5 to 12*   |
| Limestone preparation building | 0.5 to 12*   |

\*If differential pressure is less than 2 inches or greater than 10 inches, work orders will be written to investigate. Dust collector may run in the 0.5 to 2 or 10 to 12 range if reason is known. Intermittent recording of the reading is required on a monthly basis. The instrument shall be calibrated against a primary standard annually. Preventive maintenance shall be done quarterly on each baghouse..

C. Each Auxiliary Boiler (Rated at 166 x 10<sup>6</sup> Btu/hr)

| <u>Pollutant</u> | <u>lb/ 10<sup>6</sup> Btu heat input</u> | <u>lbs/hr*</u> |
|------------------|--|----------------|
| PM <sub>10</sub> | 0.10                                     | 20             |
| SO <sub>2</sub>  | 0.69                                     | 100            |
| NO <sub>x</sub>  | 0.35                                     | 58             |



\*Testing shall be done in accordance with the requirements from the most current Title V permit.

**D. Each Main Boiler Stack**

Pollutant                      lbs/hr\*,\*\*

CO            1320 lb/hr rate

\* Only for Boiler 2 Initial test is required for the verification of the overfire air system CO and O<sub>2</sub> dependency relationship developed by IPSC. \*\* After the initial test for Boiler 2 and for Boiler 1, CO compliance demonstration shall be performed once a month using the following formula developed during the testing and provided in the Babcock Power Interface "Report on Good Combustion Practices" for the IGS Unit 1.

The emission limit is verified by the conversion to pounds per hour, calculated as:

$$[C_{lb/hr}] = [C_{ppmvd}] * 2.59 * 10^{-9} * MW * F_d * 20.9 / (20.9 - O_2\%) * H_i$$

where;  $[C_{lb/hr}]$  = pound per hour emission rate  
 $[C_{ppmvd}]$  = CO concentration in parts per million, derived below  
 $2.59 * 10^{-9}$  = conversion factor for pound per standard cubic feet  
 MW = molecular weight of CO  
 $F_d = \square F \square$  factor to convert standard cubic feet per million BTU heat input.  
 $O_2\%$  = excess combustion oxygen, in percent  
 $H_i$  = heat input, in million BTU per hour

$$[C_{ppmvd}] = n \times (O_2\%)^a$$

Where:

$[C_{ppmvd}]$  = concentration of CO in parts per million volume dry  
 $n$  = curve specific factor obtained from the table below  
 $O_2\%$  = percent O<sub>2</sub> measured at the boiler stack exit <sup>1</sup>  
 $a$  = curve specific exponent obtained from the table below

Values for n and factors

|                     | <u>n</u> | <u>a</u> |
|---------------------|----------|----------|
| No OFA <sup>2</sup> | 47259    | -7.6817  |
| 1/3 OFA             | 66265    | -7.9824  |
| 2/3 OFA - throttled | 4029.2   | -4.0112  |
| 2/3 OFA - full open | 1372.4   | -3.0919  |

<sup>1</sup> For O<sub>2</sub>, Plant Information system records shall be used (which contains recorded data collected from boiler O<sub>2</sub> measurement instruments).

<sup>2</sup> OFA position shall be obtained from the recorded Plant Information system

#### E. Notification

The Executive Secretary shall be notified at least 30 days prior to conducting any required emission testing. A source test protocol shall be submitted to DAQ when the testing notification is submitted to the Executive Secretary.

The source test protocol shall be approved by the Executive Secretary prior to performing the test(s). The source test protocol shall outline the proposed test methodologies, and stack to be tested. A pretest conference shall be held, if directed by the Executive Secretary.

#### F. Sample Location

The emission point shall be designed to conform to the requirements of 40 CFR 60, Appendix A, Method 1, or other methods as approved by the Executive Secretary. Access that meets the standards of the Occupational Safety and Health Administration (OSHA) or the Mine Safety and Health Administration (MSHA) shall be provided.

#### G. Volumetric Flow Rate

40 CFR 60, Appendix A, Method 2

#### H. PM<sub>10</sub>

Compliance determination procedures and stack testing shall be performed according to 40 CFR 60, Appendix A, Method 5B.

#### I. Carbon Monoxide (CO)

40 CFR 60, Appendix A, Method 10, or other testing methods approved by the Executive Secretary.

#### J. Nitrogen Oxides (NO<sub>x</sub>)

40 CFR 60, Appendix A, Method 7, 7A, 7B, 7C, 7D, 7E, or other testing methods approved by the Executive Secretary.

#### K. Calculations for Test Results

To determine mass emission rates (lb/hr, etc.) the pollutant concentration as determined by the appropriate methods above shall be multiplied by the volumetric flow rate and any necessary conversion factors determined by the Executive Secretary, to give the results in the specified units of the emission limitation.

L. Existing Source Operation

For an existing source/emission point, the production rate during all compliance testing shall be no less than 90% of the maximum production achieved in the previous three (3) years.

11. Visible emissions from the following emission point sources shall not exceed the following values:
  - A. All abrasive blasting - 40% opacity
  - B. Main Boilers – 20% (six minute average) except for one six minute period per hour of not more than 27%. (See Title V II.B.2.3)
  - C. Emergency Diesel Generators – 20% except for start-up or shut down and for operation not exceeding three minutes in any hour. (See Title V II.B.3.b)
  - D. Diesel Driven Fire Pumps – 20% except for start-up or shut down and for operation not exceeding three minutes in any hour. (See Title V II.B.5.b)
  - E. All other points - 20% opacity

Opacity observations of emissions from stationary sources shall be conducted according to 40 CFR 60, Appendix A, Method 9.

For sources that are subject to NSPS, opacity shall be determined by conducting observations in accordance with 40 CFR 60.11(b) and 40 CFR 60, Appendix A, Method 9.

12. The following consumption limit shall not be exceeded:

50,000 barrels of fuel oil consumed per calendar year in the auxiliary boilers.

To determine compliance with this annual limit, the owner/operator shall calculate a total by the January 20th of each year using data from the previous 12 months (ending with December 31). Records of consumption shall be kept for all periods when the auxiliary boilers are in operation. Consumption shall be determined by fuel oil totalizer records. The records of consumption shall be kept on a monthly basis.

13. Emergency generators shall be used for routine maintenance and electricity producing operation only during the periods when regular electric power supply is interrupted, except for routine engine maintenance and testing. Records documenting generator usage shall be kept in a log and shall show the date the generator was used, the duration in hours of generator usage, and the reason for each usage.
14. The diesel driven fire pumps shall be operated on an emergency basis only, except for routine engine and fire system maintenance and testing. Records documenting diesel driven fire pump usage shall be kept in a log and shall show the date the diesel driven fire pump was used, the duration in hours of use, and the reason for each usage.

**Roads and Fugitive Dust**

15. IPSC shall abide by the latest fugitive dust control plan submitted to the Executive Secretary for control of all dust sources associated with the Intermountain Power Generation site.

Any haul road speeds established in the plan shall be posted.

16. The facility shall abide by all applicable requirements of R307-205 for Fugitive Emission and Fugitive Dust sources.

**Fuels**

17. The owner/operator shall combust only bituminous and subbituminous coals as primary fuels and shall only use diesel oil or natural gas during the startups, shutdowns, maintenance, performance tests, upsets and for flame stabilization in the  $9,225 \times 10^6$  Btu/hr boilers. Only No. 2 oil shall be used in  $166 \times 10^6$  Btu/hr boilers. The owner/operator may fuel-blend self-generated used oil with coal at the active coal pile reclaim structure providing that self-generated used oil has not been mixed with hazardous waste.

18. The sulfur content of any fuel oil combusted shall not exceed:

- A. 0.85 lb per  $10^6$  Btu heat input for fuel oil used in the main boilers.
- B. 0.58 percent by weight for fuel oil combusted in the auxiliary boilers.

The sulfur content shall be determined by ASTM Method D-4294-89 or approved equivalent. Certification of fuel oil shall either be by IPSC's own testing or test reports from the fuel oil marketer.

**Federal Limitations and Requirements**

19. In addition to the requirements of this AO, all applicable provisions of 40 CFR 60, New Source Performance Standards (NSPS) Subpart A, 40 CFR 60.1 to 60.18 and Subpart Da, 40 CFR 60.40a to 60.49a (Standards of Performance for Electric Utility Steam Generating Units for Which Construction is Commenced After September 18, 1978) and Subpart Y, 40 CFR 60.250 to 60.254 (Standards of Performance for Coal Preparation Plants) apply to this installation.
20. In addition to the requirements of this AO, all applicable provisions of 40 CFR Part 72, 73, 75, 76, 77, and 78 - Federal regulations for the Acid Rain Program under Clean Air Act Title IV apply to this installation.

**Records & Miscellaneous**

21. At all times, including periods of startup, shutdown, and malfunction, owners and

operators shall, to the extent practicable, maintain and operate any equipment approved under this AO including associated air pollution control equipment in a manner consistent with good air pollution control practice for minimizing emissions. Determination of whether acceptable operating and maintenance procedures are being used will be based on information available to the Executive Secretary which may include, but is not limited to, monitoring results, opacity observations, review of operating and maintenance procedures, and inspection of the source. All maintenance performed on equipment authorized by this AO shall be recorded, and the records shall be maintained for a period of two years.

22. The owner/operator shall comply with R307-150 Series. Inventories, Testing and Monitoring.
23. The owner/operator shall comply with R307-107. General Requirements: Unavoidable Breakdowns.

#### **Monitoring - Continuous Emissions Monitoring**

24. The owner/operator shall install, calibrate, maintain, and continuously operate a continuous emissions monitoring system (CEMs) on the main boilers stacks and SO<sub>2</sub> removal scrubbers inlets. The owner/operator shall record the output of the system, for measuring the opacity, SO<sub>2</sub>, NO<sub>x</sub>, CO<sub>2</sub> emissions. The monitoring system shall comply with all applicable sections of R307-170, UAC; and 40 CFR 60, Appendix B.

All continuous emissions monitoring devices as required in federal regulations and state rules shall be installed and operational prior to placing the affected source in operation.

Except for system breakdown, repairs, calibration checks, and zero and span adjustments required under paragraph (d) 40 CFR 60.13, the owner/operator of an affected source shall continuously operate all required continuous monitoring devices and shall meet minimum frequency of operation requirements as outlined in 40 CFR 60.13 and Section UAC R307-170.

25. In order to demonstrate that the modifications approved in DAQE-049-02 did not result in significant emissions increases (as defined in R307-101-2), the rolling 12-month period (that is compiled quarterly) main boilers 1&2 fuel consumption data (MMBtu/hr) and emissions from their stack flues shall be monitored for at least 5 years from the date the units begin fully using the modifications described therein as regular operation. If IPSC fails to comply with the reporting requirements of the WEPCO rule or if the submitted information indicates that emissions have increased above the significant emission increases as a consequence of the change, IPSC will be required to obtain a PSD permit for these modifications at that time. Records of NO<sub>x</sub> and SO<sub>2</sub> shall be obtained through the use of a CEM. Records of PM<sub>10</sub> shall be based on annual stack tests outlined in the Condition 9. Records for the rest of pollutants, except CO, shall be based on the EPA's Compilation of Air Pollutant Emission Factors (AP-42), industry

specific published emission factors (such as Electric Power Research Institute, Edison Electric Institute or IPSC own testing).

The Executive Secretary shall be notified in writing if the company is sold or changes its name.

This AO in no way releases the owner or operator from any liability for compliance with all other applicable federal, state, and local regulations including R307.

A copy of the rules, regulations and/or attachments addressed in this AO may be obtained by contacting the Division of Air Quality. The Utah Administrative Code R307 rules used by DAQ, the Notice of Intent (NOI) guide, and other air quality documents and forms may also be obtained on the Internet at the following web site: [http://www.eq.state.ut.us/eqair/aq\\_home.htm](http://www.eq.state.ut.us/eqair/aq_home.htm)

The annual emission estimations below include point source, fugitive emissions, fugitive dust and do not include road dust, tail pipe emissions, grandfathered emissions etc. These emissions are for the purpose of determining the applicability of Prevention of Significant Deterioration, nonattainment area, maintenance area, and Title V source requirements of the R307. They are not to be used for determining compliance.

The Potential To Emit (PTE) emissions for the IPSC power generation plant are currently calculated at the following values:

|    | <u>Pollutant</u>   | <u>Tons/yr</u> |
|----|--------------------|----------------|
| A. | PM <sub>10</sub>   | 3,286.7        |
| B. | SO <sub>2</sub>    | 11,332.3       |
| C. | NO <sub>x</sub>    | 37,868.2       |
| D. | CO                 | 11,692.3       |
| E. | VOC                | 63.91          |
| F. | HAPs               | 82.67          |
|    | Lead               | 0.39168        |
|    | Beryllium          | 0.00892        |
|    | Mercury            | 0.3135         |
|    | Fluorides (HF)     | 16.8           |
|    | Sulfuric Acid      | 8.8            |
|    | Other non-VOC HAPs | 93.2           |